

56/103

.R. LIBRARY

DEPARTMENT OF SCIENTIFIC AND INDUSTRIAL RESEARCH AND FIRE OFFICES COMMITTEE JOINT FIRE RESEARCH ORGANIZATION

23 10 1557 ...

This report has not been published and should be considered as confidential advance information. No reference should be made to it in any publication without the written consent of the Director, Fire Research Station, Boreham Wood, Herts. (Telephone: EIStree 1341 and 1797.)

THE FLARABILITY OF FABRICS -

D. I. Lawson, M.Sc., M.I.E.E., F.Inst.P.

Summary

The measurement of the speed of propagation of flame over fabrics is discussed and some general relations between flame speed and the weight of the fabric per unit area are described. Methods are outlined for the measurement of vertical flame speed with simple robust apparatus. A survey is described by which it is hoped to examine the relation between the incidence and severity of burning accidents and the vertical flame speed of the materials involved.

October, 1956 File No. 1040/32/21

Fire Research Station, Boreham Wood, Herts.

by

D. I. Lawson, M.Sc., M.I.E.E., F.Inst.P.

INTRODUCTION

Textiles are flexible woven materials. The spinning and weaving processes associated with their manufacture ensure that the finished materials are more or less a well aerated mass with good thermal insulating properties; unfortunately, this leads to conditions which are favourable to ignition and to the propagation of flame. Textiles, being flexible and subject to the usual gravitational forces, usually hang vertically; it is in this position that flame is most readily propagated and the heat transfer from the flame to the unburnt fabric ahead of the flame is greatest.

MEASUREMENT OF VERTICAL FLAME SPEED

In assessing the danger of any fabric, it will be necessary to measure the vertical flame speed, as this is a measure of the time available, either for extinguishing the flames or for discarding the burning fabric. As burning is a continuous process of ignition, any such measurement will also take into account the ease of ignition of fabrics.

It is not easy to measure vertical flame speed over fabrics directly as the flame front is not well defined. It is, however, possible to measure the vertical flame speed indirectly by weighing the fabric continuously on a torsion balance while it is burning (1). The vertical flame speed is readily calculated from the rate of loss of weight, the initial weight of the fabric and the weight of the residue. The apparatus is shown in Figure 1, and some typical results are given in Tables 1, 2, 3, 4 and 5, relating respectively to cotton and viscose rayon, acetate rayon, wool, nylon and miscellaneous fabrics.

All cellulosic materials, wood, paper and textiles, propagate flame at a rate which is inversely proportional to their weight per unit area, as shown in Figure 2. In fact, a useful formula to have in mind for cotton and viscose rayon fabrics is:-

WV = 9.3

where W is the weight in oz/yd² and V is the vertical flame speed in in./s.

It may be shown, without much difficulty, that a relation of this kind might be expected on theoretical grounds.

The corresponding expressions for other fibres have been determined with less precision because up to the present it has not been possible to test such a wide range of materials as with cellulosic fabrics, but the following relations are put forward tentatively:-

WV = 5 (acetate rayon)
WV = 8 (wool/cotton mixtures containing up to 60 per cent wool).

These figures would indicate that wool/cotton mixtures are about as flammable as, while acetate rayons are markedly less flammable than, cotton and viscose rayons of comparable weight.

The lower flame speed of acetate rayons is due to the fact that they melt and drip during burning and as each burning drip falls the flame front is momentarily checked, some of the heat from combustion being removed.

The data for the burning of wool do not permit a weight-velocity relation to be estimated but the figures which are available are not inconsistent with the flame speed being 2-3 times less than that for comparable weights of cotton.

Fabrics comprising mixtures of fibres have a flammability intermediate between that of the two fibres and very often characteristic of the more flammable of the fibres. Pure nylon and Terylene do not propagate flame continuously in a vertical direction. Nylon nets stiffened with melamine resins however propagate flame with the same velocity as cotton nets.

SEMI-CIRCULAR TEST

The torsion balance apparatus is, of course, quite unsuitable for everyday use, and this has led to the development of simpler apparatus (Figure 3) consisting of a semi-circular arched track over which the fabric to be tested is stretched. The sample is lit at one end and the final distance of burning D is noted, together with the time taken T. From these two quantities the vertical flame speed V, as measured by the torsion balance, can be estimated from the expression, shown graphically in Figure 4:-

$$V = \frac{0.31 \, D^2.5}{T}$$

The correlation between the vertical flame speed calculated in this way, and with that measured using a torsion balance is shown in Figure 5.

The semi-circular apparatus is described in B.S. 476: Part $2^{(2)}$, in which a figure of merit, M, is assigned to the sample under test. This is the time taken for flame to propagate 100 in. vertically, and it is derived from the distance and time of burning by the expression:-

$$M = \frac{320 \text{ T}}{D^2 \cdot 5}$$

which is shown graphically in Figure 6. Typical values for various materials are shown in Tables 1, 2, 3, 4 and 5.

THE 45° TEST

The speed of propagation along materials sloping at an angle of 45° has been adopted as a criterion of flammability in the United States. Experiments have been carried out at the Fire Research S ation in this way and it has been found possible in some cases to correlate the speed of burning with the vertical flame speed and hence with the figure of merit. Some typical figures are shown in Tables 1, 2, 3, 4 and 5. These have been found by measuring the time T for the flame to spread a distance of 5 in. along the slope and substituting in the empirical expression:

$$M = 2.5 T$$

The method of ignition specified in the American Federal Test is such that not all materials which permit the propagation of flame at 45° are ignited by the standard source, and in the experimental results quoted in Tables 1, 2, 3, 4 and 5, the igniting source was allowed to play on the fabric considerably longer than in the American specification. For some of the less flammable materials propagation along a 45° slope does not take place but nevertheless they will burn in the vertical direction owing to the more efficient heat transfer from the flames to the material. This will mean that there is a maximum figure of merit which can be measured on the American type of apparatus; the value of this maximum is not at present known.

DISCUSSION OF SEMI-CIRCULAR AND 45° TESTS

It will be seen on reference to Table 1 that both the semi-circular and 45° tests give a fair measure of the figure of merit of fabrics as determined by the vertical flame speed.

Both tests give figures of merit for acetate rayon considerably lower than those calculated from the vertical flame speed. This is undoubtedly due to the fact that the better support given to the fabrics in these tests as compared with the vertical test considerably reduces the dripping of the burning material.

The factor is also generally present when the tests are applied to woollen fabrics.

Pure nylon and Terylone fabrics do not propagate flame in the vertical direction and therefore would have an infinite figure of merit as determined by the vertical flame speed. The 45° test would also give this value as flame would not be propagated along the 45° slope.

The semi-circular test gives a finite figure of merit of several hundred as this is measured by both the distance and time of spread and a certain limited amount of flaming does take place near to the igniting source.

The same remarks would apply to all fabrics which do not propagate flame vertically including those receiving a number of proprietary flame-retardant treatments. When such fabrics have been laundered many times they will propagate flame slowly in the vertical direction and it is very doubtful whether propagation would take place at an angle of 45°. Under these conditions the semi-circular test is probably a more accurate measure of the figure of merit as determined by the vertical flame speed.

BURNS IN RELATION TO THE FIGURE OF MERIT OF FABRICS

In order to obtain information on the relation between the figure of merit and burning accidents, the Ministry of Health has been asked if it would enlist the co-operation of the Burns Units of hospitals in Great Britain in supplying both information regarding the accident and a sample of the fabric first ignited. The questionnaire in use is shown in Figure 7. This is printed on the back of the envelope into which a sample of fabric is placed.

When the envelope is received at the Fire Research Station, the figure of merit of the fabric is measured and recorded. The information is then coded onto punched cards by the Statistical Section.

From this survey it is hoped to answer three main questions :-

- (1) What is the distribution of the number of burning accidents in relation to the figure of merit of the fabrics first ignited?
 - (2) Is there any correlation between the extent and severity of burns and the figure of merit of the fabric involved?
- (3) What would be the effect on the pattern of burning accidents of encouraging the use of garments having a figure of merit higher than those in use at present?

From an examination of the fabrics received so far from hospitals and from the Fire Brigades, it has been possible to prepare a distribution diagram of the number of burning accidents with respect to the figure of merit of the materials first ignited. The distribution diagram is shown in Figure 8, where it will be seen that the bulk of the accidents involve fabrics having figures of merit in the range 25 - 65; this is in part due to the frequency with which such fabrics are worn. The more flammable fabrics are not responsible for the bulk of burning accidents, probably because they are not so frequently used or because such light-weight materials are usually worn in summer when fires are not generally required. Whatever the cause, the implication is clear, that it would be useless to prohibit only the most flammable fabrics as has been done in the United States.

It is probable that it would be more profitable to encourage the use of flame-retardant treated fabrics. Those now on the market and those likely to be produced within the next year have figures of merit of several hundreds, and the treatments resist laundering as well. Unfortunately, the cost of these is a big obstacle in the way of their general adoption. It has been suggested (3) that the increased cost of producing flame-retardant treated fabrics might be offset by a subsidy as their general use would reduce the expenditure by the Health Services in treating burns cases. Before this could be done it would be necessary to estimate the effect of changing the clothing habits of the nation on the number and severity of burns. This is a difficult problem but it is made easier to some extent by the fact that burning accidents are confined mainly to dresses and nightdresses.

The collection of the statistical evidence correlating the figure of merit with severity and occurrence of burns will take some time. If in the meantime it were felt that some administrative action were necessary, a British Standard could be drawn up for fabrics having a flammability so low that burning accidents would be unlikely. The figure of merit for such fabrics would be considerably greater than that of the fabrics normally used in clothing. In fixing such a limit two factors would have to be considered:-

- (1) The speed of flame propagation along the fabric. Materials only propagating flame slowly would be unlikely to cause severe burns and such flaming would be readily extinguished.
- (2) The figure of merit. This, if the Standard were to be of any practical use would have to be attainable commercially, even after repeated laundering, representing the normal life of the fabric.

If such a standard of performance were defined it would have the immediate advantage of providing the public with materials unlikely to cause serious burns casualties and would also provide industry with an agreed basis for development.

Colebrook and Colebrook have repeatedly pointed out ⁽⁴⁾ that the first tasks are to see that all open fires are guarded and that flowing nightwear for children should be avoided. Parents can be urged to take these measures now and until such time as flame-retardant treated fabrics are generally available.

REFERENCES

国际主意经济 鬼

- 1) LAWSON, D. I., WEBSTER, C.T. and GREGSTEN, M. J. The flammability of fabrics. J. Text. Inst., 1955, 46 (7) T453-T463.
- 2) Flammability test for thin flexible materials. British Standard 476: Part 2: 1955.
- 3) COLEBROOK L. et al. The prevention of burning accidents. Brit. med. J., 1956, 1 (4930) 1379-86.
- 4) COLEBROOK, L. and COLEBROOK, V. The prevention of burns and scalds.
 Lancet, 1949, 2 (6570) 181-8.

| Description | Weight per unit area oz/yd ² W | Vertical flame speed in./s | Figure of merit $M = \frac{100}{V}$ | Figure of merit Semi-circular test | Figure of merit American test | |
|--------------------|--|----------------------------------|-------------------------------------|---|--|--|
| Viscose net | 0.5 | 13 | 7.7 | 8 | 7 | |
| Viscose net | 0,5 | 16 | 6.3 | 6 | 7 | |
| Viscose net | 0.7 | 9.4 | 10.6 | 9 | 10 | |
| Cotton net | 0.8 | 14 | 7.2 | 7 | 8 | |
| Cotton muslin | 1.0 | 6.0 | 16 | 9 | 8. | |
| Cotton net | 1.3 | 18 | 5,6 | 6 | 8 | |
| Viscose | 1.8 | 6,1 | 16 | 20 | <u>.</u> | |
| Cotton | 1.9 | 3.5 | 29 | 17 | 14 | |
| Viscose ninon | 1.9 | 4.8 | 21 | 21 | 14 | |
| Cotton seersucker | 2,3 | 3,2 | 31 | 21 | •••••••••••••••••••••••••••••••••••••• | |
| Cotton | 2.4 | .3.4 | 29 . | 22 | 18 | |
| Cotton gingham | 2.8 | 2.8 | 36 | 26 | 22 | |
| Viscose | 3.0 | 2.9 | 35 | 37 | - | |
| Viscose | 3.3 | 2.7 | 37 | 30 | ••• | |
| Cotton | 3,6 | 2.5 | 40 | 33 | 30 | |
| Cotton poplin | 3.8 | 2,4 | 42 | 36 | | |
| Cotton, embossed | 3.9 | 2,4 | 42 | 30 | ' | |
| Cotton winceyette | 3,9 | 2.0 | 50 | 31 | 33 | |
| Cotton winceyette | 4.0 | 2.2 | 45 | 34 | - | |
| Cotton | 4.1 | 1.7 | 59 | 33 | 45 | |
| Cotton | 4.1 | 1.9 | 53 | 33 | 48 | |
| Cotton | 4.3 | 2.8 | 36 | 32 | - | |
| Cotton flannelette | 4.3 | 2.4 | 42 | 3 5 | | |
| Cotton | 4.6 | 2.0 | 50 | 38 | 34 | |
| Cotton, viscose | 4.6 | 1.9 | 53 | 39 | 36 | |
| Viscose locknit | 4,6 | 1.9 | 53 | 56 | 42 | |
| Viscose lambspun | 4.8 | 1.9 | 53 | 56 | 44 | |
| Cotton cambric | 5.6 | 1.8 | 56 | 46 | _ | |
| Viscose, brushed | 5,6 | 1.9 | 53 | 51. | 53 | |
| Viscose | 5.6 | 1.6 | 63 | 67 | - . | |
| Viscose, brushed | 5,9 | 2.0 | 50 | 49 | - | |
| Cotton velveteen | 6.3 | 1.9 | 53 | 50 | <u>`</u> | |

TABLE 1 (contid) FLAME SPREAD OVER COTTON AND VISCOSE RAYON

| Description | Weight per unit area oz/yd ² W | Vertical flame speed in./s | Figure of merit M= 100 V | Figure of merit Semi-circular test | Figure of merit American test |
|--------------------------|--|----------------------------------|---------------------------|---|--|
| Cotton furnishing fabric | 7.3 | 1.4 | 71 | 60 | · - |
| Cotton velour | 7.5 | 1.3 | 77 | 70 | - |
| Viscose | 8,1 | 1.1 | 91 | 80 | |
| Viscose, brushed | 8,5 | 2,3 | 43 | 48 | 19 |
| Cotton corduroy | 8.9 | 1.4 | 71 | 65 | |
| Cotton loomstate weave | 10.8 | 0,92 | 109 | 71 | : # * |
| Cotton towelling | 14.7 | 1.0 | 100 | 67 | estee |

...

TABLE 2 - FLAME SPREAD OVER ACETATE RAYON

| Description | Weight per Vertical unit area oz/yd ² flame specin./s | | Figure of merit | Figure of merit | Figure of merit |
|------------------------|--|------|-----------------|-----------------------|------------------|
| | | Λ. | M = 100 | Semi-circular test | American test |
| Acetate rayon | 1.7 | 1,7 | 59 | 10 | 16 |
| Acetate rayon | 1.7 | 1.9 | 53 | 11 | · = · |
| Acetate rayon | 2,3 | 1,5 | 67 | 9 | . 16 |
| Acetate rayon | 2.8 | 1.7 | 59 | 18 | 18 |
| Acetate rayon lingerie | 2,9 | 2,1 | 48 | 30 | 23 |
| Acetate rayon lingerie | 2,9 | 1.9 | 53 | 26 | 23 |
| Acetate rayon lingerie | 3.6 | 1.5 | 67 | 22 | 22 |
| Acetate rayon lingerie | 3. 8 | 1.4 | 71 | 23 | 21. |
| Acetate rayon satin | 4.9 | 0,87 | 115 | - 22 | 27 |
| Acetate rayon twill | 6.9 | 0,90 | 111 | 42 | 38 |

TABLE 3 - FLAME SPREAD OVER WOOL

| Description | Weight per unit area oz/yd² W | Vertical flame speed in./s | Figure of merit $M = \frac{100}{V}$ | Figure of merit Semi-circular test | Figure of merit American test |
|---------------|--|----------------------------------|-------------------------------------|---|--|
| Wool | 3.7 | 0,69 | 145 | 47 | gwa : |
| Wool | 3.9 | 0.81 | 124 | 47 | Project. |
| Wool | 5,6 | 0.69 | 145 | 49 | \ |
| Wool | 7.5 | 0.31 | 323 | 136 | - |
| Wool | 7.8 | 0.68 | 147 | 159 | sooji |
| Wool, knitted | 8.1 | 0 | ⇔ | 105 | ent . |
| Wool serge | 13.7 | 0 | ∞ ∞ | over 200 | |
| Wool serge | 18,6 | 0 | 00 1 | over 200 | ons . |

TABLE 4 $\stackrel{\text{\tiny def}}{=}$ FLAME SPREAD OVER NYLON

| Description | Weight per unit area oz/yd ² | Vertical flame speed in./s | Figure of merit M = 100 V | Figure of merit Semi-circular test | Figure of merit American test |
|-------------|---|----------------------------------|----------------------------|---|---|
| Nylon net | 0.4 | 3.3 | 30 | 8 | |
| Nylon net | 0.4 | <u> </u> | _ | 8 | - |
| Nylon net | 0.4 | 2.7 | 37 | 8 | - |
| Nylon | 1.1. | o'. | , ∞ | over 200 | |
| Nylon | 1.4 | 0 | 000 | over 200 | - |
| Nylon | 1.4 | 0 | ∞* | over 200 | _ |
| Nylon | 1.6 | 0 | ∞ . | over 200 | |
| Nylon | 1.9 | 0 | ∞: | over 200 | |
| Nylon | 2,0 | 0 | ∞ | over 200 | - * · · · · · · · · · · · · · · · · · · |
| | | | - | | i kato i ji |

TABLE 5 - FLAME SPREAD OVER MISCELLANEOUS FABRICS

| Anna and the regulation design of the second | and the state of t | | | | and the second s |
|--|--|----------------------------------|-------------------------------------|---|--|
| Description | Weight per unit area oz/yd ² W | Vertical flame speed in./s | Figure of merit $M = \frac{100}{V}$ | Figure of merit Semi-circular test | Figure of merit American test |
| 200/7 200/ | 2 7 | 1,8 | 56 | 58 | and the state of t |
| 20% wool 80% cotton 20% wool 80% cotton | 3.7 4.0 | 2.1 | 48 | 44 | 76 |
| 40% wool 60% cotton | 3.5 | 2.2 | 45 | 42 | |
| 40% wool 60% cotton | 4.4 | 2.0 | 50 | 46 | - |
| 50% wool 50% viscose | 7.7 | 0.67 | 149 | 336 | - |
| 55% wool 45% cotton | 3,9 | 2.0 | 50 | 51 | |
| 60% wool 40% cotton | 3.7 | 2.3 | 44 | 52 | <u></u> |
| 60% wool 40% cotton | 4.1 | 1.7 | 59 | 71 | · - |
| 50% wool 50% nylon | 8.5 | 0 | . ∞ | 194 | |
| 50% wool 33% viscose 17% nylon | 7,7 | 0.47 | 213 | 100 | |
| 50% wool 33% nylon 17% viscose | 8,6 | 0 | ∞: | 435 | - |
| Linen crash | 5.4 | 2.1 | 48 | 43 | - |
| Winceyette: 50% Fibros 33% viscosel6.2/3rds nylon | ceta 3,9 | 1.1 | 91 | 50 | |
| Wool-Orlon | 6.4 | 1.1 | 91 | 120 | - |
| Wool-polyacrylonitril | 9 8.7 | 0,8 | 125 | 90 | - |
| Cotton, Erifon treated | 5.9 | 0 | 00 | over 200 | mai |
| Cotton, Erifon treated | 6.3 | 0 | ∞ | over 200 | , |
| Cotton, Erifon treated | 8,5 | 0 | ∞. | over 200 | - |
| Canvas, Erifon treated | 15.3 | 0 | ∞ | over 200 | - |
| Cotton, Proban treated | 5.1 | 0 | ∞ | over 200 | |
| Viscose, Proban treate | d 8.5 | 0 | ∞ | over 200 | - |
| Canvas, Proban treated | 9.9 | 0 | ∞ | over 200 | po l |
| Cotton twill, Proban treated | 12.2 | 0 | ∞ | over 200 | |
| 67% viscose 33% Fibro | lane 5.4 | 1.8 | 56 | 83 | |
| 67% viscose 33% Fibrolane 5.6 | | 1.6 | 63 | 88 | - |
| 67% viscose 33% Fibrolane 7.4 | | 1,3 | . 77 | 101 | - |
| 67% viscose 33% Fibro | lane 9,1 | 1.4 | 71 | 99 | - |
| Viscose -Orlon | 8.7 | 1.8 | 56 | 68 | - |
| Viscose - Terylene | 9.0 | 1.0 | 100 | 80 | |
| | | | | L | |

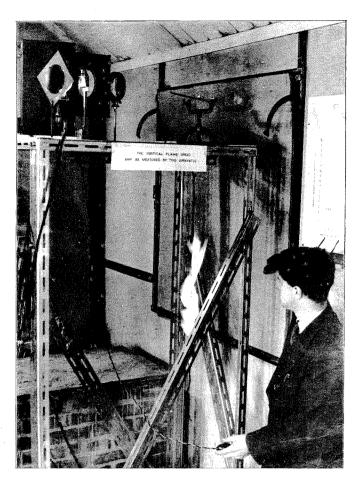


FIG.I. APPARATUS FOR MEASURING VERTICAL FLAME SPEED

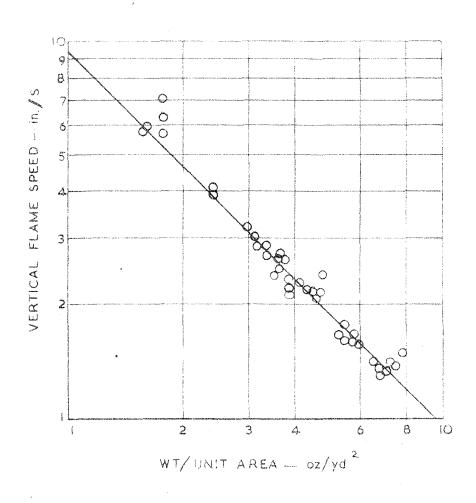


FIG.2 RELATIONSHIP BETWEEN VERTICAL FLAME SPEEL (V) AND WT PER UNIT AREA (W) FOR CELLULY MIC MATERIALS

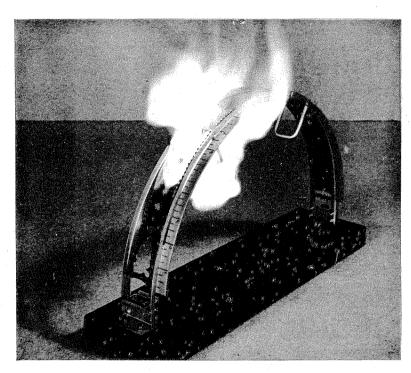
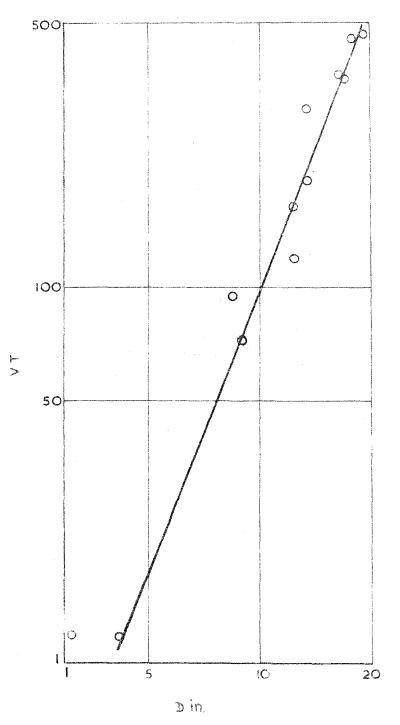


FIG. 3. SEMI-CIRCULAR APPARATUS FOR CLASSIFYING FABRICS



VT = 0.31D^{2.5}
V = vertical flame speed in in./s
T = time in sec to spread distance D in

FIG. 4 ESTIMATION OF VERTICAL FLAME SPEED

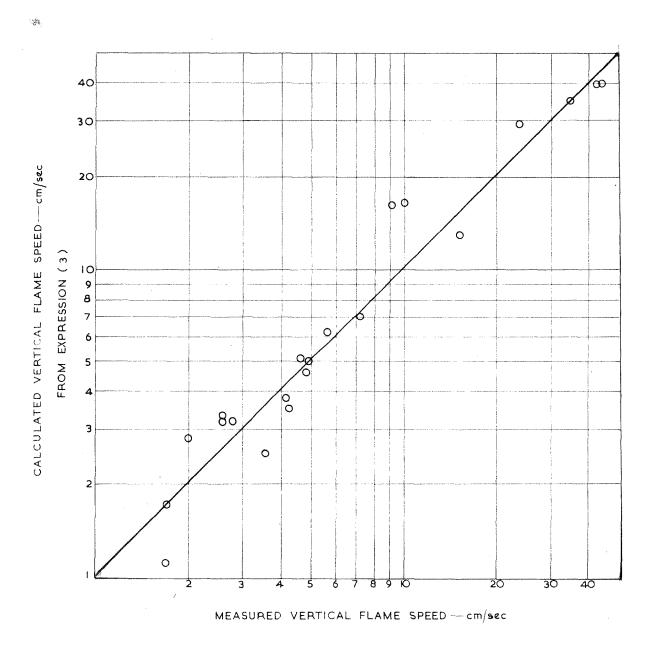


FIG. \$ COMPARISON OF MEASURED AND CALCULATED VERTICAL FLAME SPEEDS

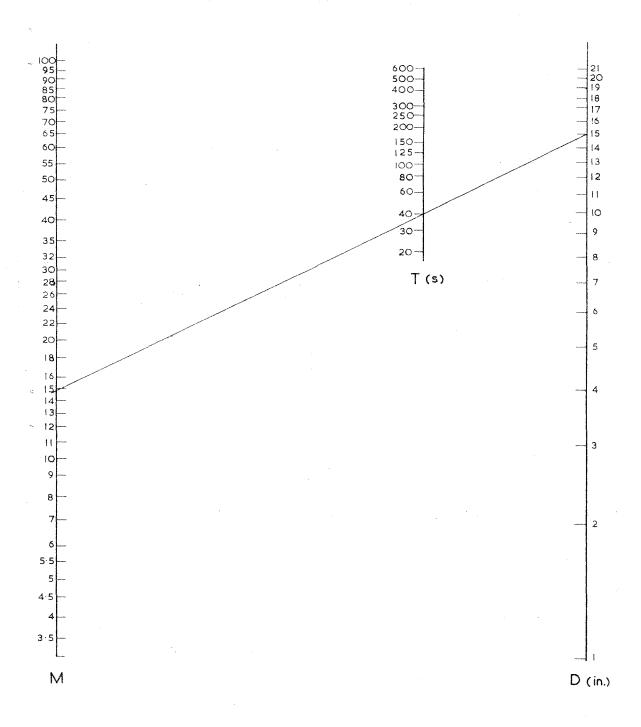


FIG. 6. NOMOGRAM OF $M = \frac{320 \text{ T}}{D^{2-5}}$

gu bu

DEPARTMENT OF SCIENTIFIC AND INDUSTRIAL RESEARCH AND FIRE OFFICES COMMITTEE JOINT FIRE RESEARCH ORGANIZATION Station Read, Borcham Wood, Horts. REPORT FORM FOR INVESTIGATION ON BURNS DUE TO FABRICS (For notes on completing form see back of cavelope)

COLS CODE ITEM ITEM LOCATION OF ACCIDENT
At home
At work
Out of doors
Elsewhere
Unknown
SOURCE OF IGNITION SEX SOURCE OF IGNIT
Open coal fire
Ges fire
Electric fire
Old stove
Closed stove (coal
or coke)
Gas cooker or ring
Electric cooker or
ring
Smoking muterials
Matches
Matches children
playing with
Candle or taper
Other than above 40-41 01 02 03 04 05 TYPE OF CASUALTY 15
Fatal
Non-fatal Non-Intal
PARTS OF BODY
BURNED
(Indicate all
parts burned)
Head
One urm
Both arms
One leg
Both legs
Trunk, lower front
Trunk, lower front
Trunk, lower back
Trunk, lower back 16 17 99 Unknown THIS SECTION FOR USE OF
FIRE RESEARCH STATION

FABRIC

Type
Wv/cm2(tmg)
Distance of
spread
Time round whole
are (see)
Vert. flame
speed (cm/see) 28-29 30-31 32-33 Trunk, lower back
AREA OF BURNS
(% of body area)
Less than 5%
5-10%
10-15%
12-20%
22-23%
23-30%
30-35%
35-40%
40-45%
More than 50% Unknown 23-24 USE OF CUARDS (Complete if source) of ignition was any heating appliance) Cuard in use Cuard not in use 42 34-36 37-38 speed (cm/sec) Unknown Unknown
ASSISTANCE TO INJURED
PERSON
Other persons present
to assist
No one present to
assist
Unknown
Remarks 43 2 DEPTH OF BURN
Full skin thickness
Partial skin
thickness 25

FIG.7. REPORT FORM FOR INVESTIGATION OF BURNS DUE TO FABRICS

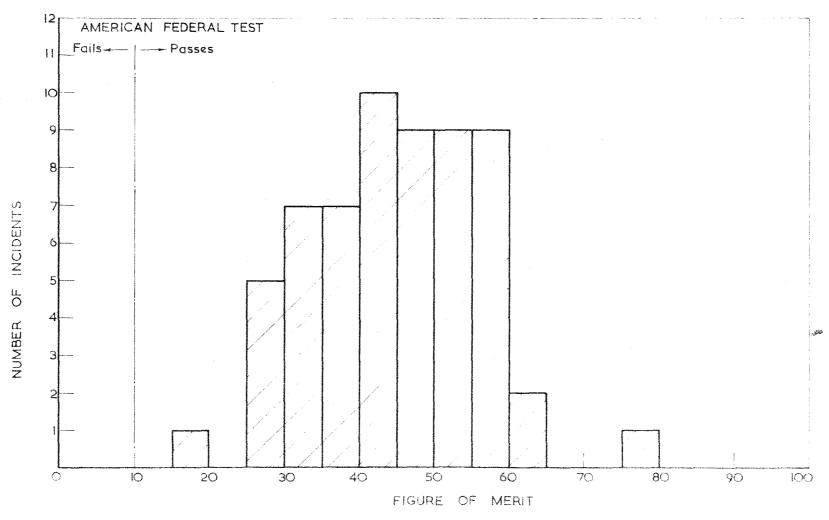


FIG. 8. VARIATION OF NUMBER OF INCIDENTS WITH FIGURE OF MERIT INCLUDING R.F.I.B. INCIDENTS AND ALL OTHERS.